ROTARY ULTRASOUND SCANNER FOR SOFT TISSUE EXAMINATION

This application is a continuation of U.S. Patent Application No. 10/263,758 filed on October 4, 2002.

BACKGROUND OF THE INVENTION

FIELD OF THE INVENTION

[0001] The present invention relates in general to medical imaging systems and to a rotary ultrasound scanner for soft tissue examination for use in such systems.

DESCRIPTION OF THE PRIOR ART

[0002] Medical imaging is an important aspect in the practice of medicine. The use of medical imaging to assist in the diagnosis of patients has been well established over the years with different technologies being employed in scanning equipment. Current imaging technologies utilise x-rays, magnetic resonance imaging (MRI), ultrasound and other modalities to produce an image of the region of interest. However, each of these suffers from certain limitations in use. Technologies using x-rays require a limited use in a carefully controlled environment in view of the cumulative effect of radiation on the patient. Both MRI and x-ray imaging equipment are relatively immobile due to the large size of the scanning equipment. It is also frequently necessary to inject dyes (contrast media) into the patient to enhance visualisation, which, in turn, leads to the use of further specialized equipment.

[0003] The use of immobile specialized equipment makes it difficult to monitor patients frequently due to limited access to the equipment and the need to provide examination facilities. This biases the usage against frequent monitoring and evaluation of changes over time, which are particularly beneficial in the early detection of abnormalities.

[0004] The use of ultrasound devices in the examination of patients by medical practitioners has been a well-established practice since the 1950s. Ultrasound has proven to be useful in the field of medical imaging for soft tissue examination, particularly in detection of breast cancer in women. However, it has typically been used as an adjunct to mammography due to its limited scanning depth, lack of image resolution and amount of noise present in the acquired data.

Historically, ultrasound has been used post-mammography to determine whether masses in the breast are solid (requiring biopsy) or cystic (benign) but has not generally been considered to be useful in detecting masses in breast tissue that are smaller than 1 mm by 1 mm. The factors influencing this limitation are noise in the acquired data, the inability to replicate scans due to tissue deformation, and operator-dependant image interpretation. In practice, mammography has been found useful to detect microcalcifications as small as 0.3 mm. Microcalcifications generally start as small as 0.1 mm and are considered an early indication of a condition requiring ongoing monitoring.

[0005] Although there have been attempts to detect microcalcifications using ultrasound technology, it appears that most attempts have not succeeded. A discussion of ultrasound resolution can be found in the doctoral thesis of Sheila McFarland, UBC. In most of the prior art, it is believed that ultrasound is not capable of detecting microcalcifications with any degree of accuracy which has inhibited its utilisation on a broad basis.

[0006] However, the use of ultrasound does not require the elaborate safety precautions necessary with other imaging systems and therefore lends itself to frequent monitoring regimes. To be effective, a good coupling must be provided between the ultrasound transducer and the soft tissue and in some prior art scanners, the body part being examined has to be deformed prior to scanning to achieve this. This is partially to secure contact but primarily to manipulate tissues in the insonified area for best identification. Classic ultrasound may be considered a tissue manipulation practice performed with visual assistance. The deformation of the body part makes comparison of sequential images difficult, makes a read difficult to repeat and may lead to various masses being hidden from the scanner..

[0007] An ultrasound scanner for imaging breast tissue is disclosed in US Patent 6,005,916 to Johnson et al. and assigned to Techniscan Inc. This scanner utilises an annular array of transducers to interrogate an object placed within a water-filled chamber. The transducers in the annular array are operated sequentially to obtain a circumferential scan and the array is then moved vertically to perform a further scan. In this manner a 3 dimensional image may be obtained. The array may be adjusted circumferentially to adjust the position of the transducers relative to an object.

[0008] The scanner disclosed in the Johnson patent is relatively expensive due to its annular array and requires a complicated bladder arrangement for coupling the transducer to the fluid in

the examination chamber. Moreover, the Johnson patent is silent as to issues regarding repeatability of image capture such as is necessary to permit monitoring over an extended period.

[0009] It is an object of the present invention to mitigate or obviate at least one of the above-mentioned disadvantages.

SUMMARY OF THE INVENTION

[0010] In one aspect, the present invention provides a medical imaging system comprising a patient support surface. An imaging apparatus having a support table located within the support surface, and adjustable relative to the support surface to be located above the surface and thereby engage a portion of the patient to be imaged.

[0011] According to a further aspect of the present invention there is provided an ultrasound scanner assembly comprising a base, a drum rotating on the base. A transducer head rotating with the drum and displaced relative to the drum along an axis parallel to the axis of rotation. The head including a plurality of transducers each operable to propagate a wave along an axis of propagation and to receive signals from respective focal zones spaced relative to one another along the axis of propagation.

[0012] According also to the present invention there is provided a method of monitoring a medical condition through insonification with ultrasound by locating a portion of a patient on a scanner in a predetermined position to permit acquisition of date in a repeatable manner, conducting a succession of scans of the area of interest of the patient at predetermined intervals, transferring the scan to a remote location and comparing time separated scans to determine changes in said medical condition.

BRIEF DESCRIPTION OF THE DRAWINGS

[0013] An embodiment of the invention will now be described by way of example only with reference to the accompanying drawings in which:

[0014] Figure 1 is a schematic representation of components of a scanning system;

[0015] Figure 2 is a plan view of the system of Figure 1;

[0016] Figure 3 is a perspective view of a scanner assembly incorporated in the system of Figure 1;

[0017] Figure 4 is a side elevation of the scanner assembly of Figure 3;

[0018] Figure 5 is a detailed view of a portion of Figure 4.

[0019] Figure 6 is a functional block diagram of the controls used in the scanner assembly of Figure 3;

[0020] Figure 7 is a schematic representation of the data acquired after one pass of the scanner assembly of Figure 3;

[0021] Figure 8 is a flow chart representing the manipulation of data obtained from a pass of the scanner assembly of Figure 3;

[0022] Figure 9 is a schematic representation of a complete signal produced by the manipulation of data;

[0023] Figure 10 is a schematic representation of the data structure used in the manipulation process of Figure 8; and

[0024] Figure 11 is a view of an interface used to control operation of the system of Figure 1.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0025] As can be seen in Figures 1 and 2, an ultrasound scanning system **10** includes a patient examination station **12** with a patient support surface **14**. The surface **14** has an opening **16** to receive a table **18** formed by a lid **19** of a scanner assembly **20**. The table **18** may be covered with a soft or cushioning material to improve patient comfort in use if so required. Scanner assembly **20** rests within a scanner case **22** located underneath the examination station **12**. A remote computer **24**, including a data acquisition software module **25**, is connected to the scanner **20** to receive data acquired during the operation of the scanner **20**.

[0026] The scanner case **22** is supported on the floor and has an upper support base **26** to receive the scanner assembly **20**. A resilient support **28** is positioned between the assembly **20** and support base **26** to allow limited vertical movement between the base **26** and the assembly **20**. An adjustment mechanism **30** is provided for the base **26** to allow vertical adjustment of the base and thereby adjust alignment between the patient support surface **14** and the table **18** of the scanner assembly **20**. Any suitable adjustment mechanism may be used such as a rack and pinion drive or a releasable cam and slide. The scanner assembly **10** is shown in greater detail in Figures 3, 4 and 5.

[0027] The scanner assembly **20** includes a base **32** supporting a body **34**. Body **34** has sidewalls **36** that support the scanner lid 19 forming the table **18**. An aperture **40** is provided in the scanner lid **19** to receive a pendant breast of a patient prone on the support surface **14**.

[0028] A drum **42** is rotatably supported on the base **32** by a spindle **44**. The drum **42** has a peripheral sidewall **46** and an end plate **48** supported on the spindle **44**. The upper end **50** of the sidewall is received in a recess **52** in the underside of the lid **19** around the aperture **40** to locate the drum but allow rotation relative to the scanner lid **19**.

[0029] A channel **54** is formed in the sidewall **46** parallel to axis of rotation. The channel **54** supports a transducer head **56** that is moveable along the channel **54** under the control of a drive motor **58**. The motor **58** is supported on the underside of the end plate **48** and drives a pair of lead screws **60** through a toothed belt **62**. The lead screws **60** support the transducer head **56** so that rotation of the lead screws will provide translation of the transducer head **56** along the channel **54**. A switch **63** is located at an upper end of the channel **54** and is activated by the transducer head **56** to indicate an upper limit of travel.

[0030] The spindle **44** supporting the drum **42** is driven by a motor **64** secured to the base and driving the spindle **44** through a toothed belt drive **66** acting on a cog wheel **68**. The spindle **44** also carries a rotary encoder **70**, which consists of a disc **72** having alternating light and dark sectors disposed around the periphery of the disc. An optical pick-up mechanism **74** is disposed at the periphery of the encoder disc **72** to provide a signal indicative of rotation and position of the drum **42**. Each pulse of this signal marks a rotational increment. A resolution of 1800 marks has been found to be satisfactory although other resolutions might be used. The encoder disc **72** also provides a zero home position indicator that allows a reference position for the disc to be determined. The zero position is identifiable in the pulse train obtained from the encoder disc by a unique pattern. Alternatively an absolute position encoder may be used to report a crisp position pointer.

[0031] The transducer head **56** includes a substrate **80** (Figure 3) carrying three ultrasound transducers **82, 84, 86**. Each of the transducers is controlled by electronic circuitry indicated at **88** and carried on the end plate **48** of the drum **42**. Data flow and control signals to and from the transducers is transferred from the electronic circuitry **80** through slip rings **89** on the spindle **44** below the encoder disk **72** to a buffer and communication module **90** for transfer to the data acquisition module **25** on the computer **24**. It will be noted that the location of the circuitry 88 on

the rotating components enables the signals from the transducers to be processed without being subjected to the noise that may be introduced by the slip rings 89 and thereby enhance the extraction of information from the resultant signals.

[0032] The transducers **82, 84, 86** are each mounted on the substrate **80** such that there axis of propagation is inclined upwardly relative to the axis of rotation of the drum **44**. As shown in Figure 5, the angle of inclination α, measured from the horizontal is selected so that the axis of propagation is generally orthogonal to the average tangent to the surface of a breast located in the drum **44**. Typically an angle of 30° to the horizontal (i.e. 60° to the axis of the rotation) is found to be satisfactory although a range of 25 ° to 35° (55° to 65° to the axis of rotation) may be used.

[0033] Each of the transducers is also selected to provide different focal zones Z_1 Z_2 Z_3 which overlap along the axis of propagation. In a preferred embodiment transducers having a focal length of 30, 50 and 80 mm and with depths of field of 22-43mm; 14-87mm; and 44-140mm respectively are used with a drum diameter of 175 mm. The transducers have an operating frequency of 4.0 MHz. A sampling rate of 20MHz is preferred to provide an oversampling and resolution better than one half wavelength.

[0034] The functional blocks of the electrical circuitry **88** and buffer and communication module **90** are shown in Figure 6. The buffer and communication module **90** is provided on a standard parallel interface **100** for communication with the computer **24**. Overall control of the scanner assembly is provided by a control and synch module **102** that receives operational parameters from the computer **24** as will be described more fully below. The control and synch module **102** initially sets the required gain of a main amplifier **104.** Output from the main amplifier **104** is digitised by an A/D converter **118** and stored in a buffer 120 for communication over the interface **100**.

[0035] A preamplifier **106** is associated with each of the transducers **82, 84, 86** and included in the circuitry **88** carried on the end plate **48.** Input signals from the encoder **70** are processed through indexing function **107** and provided to the control and sync module **102**. Module **102** generates a trigger pulse **108** at intervals defined by the operational parameters received from the computer **24** and transfers it across the slip ring 89 to a pulse multiplexer control module **110.** The multiplexer control module **110** sequentially directs a trigger pulse signal **112** to a pulse circuit **114** associated with each of the transducers **82, 84, 86** respectively. The encoder **70** provides a pulse for each mark on the disc and, for maximum resolution, each pulse is used to

trigger one of the pulse circuits **114**. Thus for an 1800 line encoder each of the transducers is fired 600 times per revolution.

[0036] The reflected signal is received by the transducer and amplified by the corresponding preamplifier **106** before being passed to a signal multiplexer **116**. The signal multiplexer **116** is switched by the module **102** after a predefined delay so as to receive the reflected signal in the zone to be examined by the respective transducer. The delay is software adjustable depending on the volume of tissue to be scanned but delays of 30 microseconds (μs) are typical for the exemplified apparatus. Multiplexer **116** passes the composite signal to the main amplifier **104**. The amplified signal is then digitised by A/D converter **118** and stored temporarily in buffer **120**. The contents of the buffer **120** are read prior to the data being overwritten with the output from the next transducer and are downloaded through interface **100** to the data acquisition module **25** of the computer **24**.

[0037] The control and synch module **102** is also operable to identify a zero or home position on the encoder **70** and initiate operation of vertical drive motor **58** to displace the transducer head **56** by a selected distance upon completion of a circumferential scan. Thereafter further scanning in a circumferential direction is performed.

[0038] As shown schematically in Figure 7, after one revolution, the data acquisition module **25** acquires data representing a set of conical slices S_1, S_2, S_3 made up of segments **124** representing the signals obtained from transducers **82, 84**, and **86** respectively. Each subsequent scan obtains data representing an additional set of slices displaced vertically from the previous set to provide a set nested conical slices from which a three dimensional image may be generated. The data acquisition module 25 receives data including the digitised reflected signal received by each of the transducers and the circumferential and vertical position of the transducer when the signal was received. Each of the data records, therefore is a representative of the structure along respective segments 124 of the conical slices S_1, S_2, S_3, shown in Figure 7. To permit generation of a three dimensional image, the data in the data acquisition module 25 must be manipulated as set out in the flow chart of Figure 8.

[0039] As an initial step 126, the slices S_1, S_2, S_3 are aligned circumferentially using the zero reference signal obtained from the indexing function 107. As indicated in Figure 9, the segments 124 in one slice will be offset circumferentially from one segment in the adjacent slice due to the rotation of the scanner assembly. The width of the insonifying beam produces a degree of

overlap between circumferentially adjacent segments 124 which increases as the segments 124 converge toward the apex of the cone. The circumferentially adjacent segments will therefore contain common information and a comparison of the adjacent segments 124, indicated at 128 in Figure 8, permits confirmation of a detected structure and removal of noise from the received signal.

[0040] The segments 124 in each slice require further processing to take account of the different gains established in preamplifiers 106 for each of the transducers 82, 84, 86. Due to the overlapping between the focal zones the Z_1, Z_2, Z_3 of each transducer, a comparison indicated at 129 between the same signal in the overlapping portions may be used to produce a normalising multiplier to provide a common basis for the signal in each segment.

[0041] Referring therefore to Figure 9, the segments 124 for the zones Z_1 and Z_2 overlap radially as indicated at 130. The signal in each of the overlapping portions of the segments should be representative of the same structure and therefore have the same value. To compensate for signal attenuation, a weighting factor is applied as indicated by the trapezoidal envelope's 131, 132 associated with zones Z_1 and Z_2 respectively. The signal of each segment is sampled (134) at a number of locations in the overlapping portion 130 weighted (136) by the appropriate envelope 131, 132 and a comparison made between the resulting values to obtain (138) a ratio between the signals. The ratio is then applied (140) to one of the segments 124. A similar process is repeated (142) in the overlap between Z_2 and Z_3 so that the three segments representing the structure at a particular location are represented on a common basis.

[0042] The factored received signals obtained at step (140) are still influenced by the attenuation of the beam as it passes through the insonified tissue. To compensate for the attenuation in the direction of propagation, an average attenuation profile is obtained from the factored signals as indicated in Figure 10.

[0043] Initially, the contour C_0 of the surface of the breast is located by examining each composite received signal for the initial reflection. The detected contour C_0 is decreased by a predetermined offset, dr, and the average signal about the circumference of the decreased contour C_1 is obtained. The contour is further decreased by the offset dr and the average signal C_2 is obtained. This is repeated along the path of the propagation to an inner value to obtain an attenuation profile indicated in chain dot line based on the average signal. Once the profile is determined, an inverse or reciprocal of the profile is obtained and a brightening algorithm

applied to the reformatted signals to obtain a normalised set of data representative of the structure that has been insonified.

[0044] After each circumferential scan has been normalised, the data may then be converted to a 3D Cartesian representation for display.

[0045] The software application implemented by the computer **24** includes a GUI interface, shown in figure 11, permitting selection of the parameters required for the data acquisition and identification of the patient, date and similar biographical data. The parameters selected include gain control for each of the preamplifiers **106** to compensate for signal attenuation on a transducer by transducer basis as indicated at **200**; an adjustable delay period between pulse control multiplexer and signal multiplexer to compensate for different tissue sample sizes; adjustable amplification of the main amplifier **104** to compensate for tissue density fluctuations between patients indicated at **202**; adjustable vertical increments **204** at the head **56** to accommodate different pathologic conditions and adjustable horizontal scan rate **206** to optimise the data acquisition versus the time required to perform a scan. Each of these parameters is user selectable on the GUI for a particular patient and transmitted to the control and synch module **102** prior to a scan being performed.

[0046] To perform a scan the drum **42** is filled with water such that upon placement of the breast within the drum the water will be within a few mm of the top of the drum **42**. A patient is positioned on the patient support surface **14** and the scanner support base **26** adjusted so that the table **18** is slightly proud of the support surface **14**. The table **18** is positioned such that the majority of the weight of the patient is taken by the support surface **14** but there is sufficient pressure exerted on the table **18** by the patient to maintain a stable position and an acceptable level of comfort. Relative movement between the scanner and patient due to breathing or bodily movement is thus inhibited by the extra pressure exerted by the body. The patient/s breast is allowed to hang pendant within the water.

[0047] The patient's arm on the opposite side to the breast being examined may be placed above their head to increase contact, improve comfort and reduce the compression of tissue adjacent the chest cavity. After initial positioning, a visual check is made for correct positioning and a preview or test scan is initiated to confirm a proper position. Once the correct position is obtained, the patient is immobilised by padding and/or straps on the support surface **14**.

[0048] To facilitate data acquisition and identification, a pair of presence transducers **122**, typically either proximity or pressure transducers, are incorporated in the table **18** to either side of the aperture. The presence of the patient's sternum will be detected by one of the transducers **122** thereby indicating whether the left or right breast is being imaged.

[0049] The operating parameters are selected at the GUI and a scan initiated. The switch **63** ensures that the start position of head **56** is maintained for each scan. At each designated interval as identified by the encoder **70**, the respective one of transducers **82, 84, 86** is pulsed and the reflected image received and processed. The overlapping focal zones Z_1 Z_2 Z_3 ensure a complete scan along the axis of propagation. The delay between propagation and receipt of the signal at each transducer ensures that the acquisition is performed in the region of interest for each transducer in turn and that the initial large reflected signal obtained during initial pulse firing is avoided. As seen in Figure 5, the signals processed are from distal portions of the path so that the signal attenuation is minimised over the observed depth of field. This permits the gain to be adjusted to obtain optimum signal strength and thereby enhance image acquisition and for each transducer to be adjusted for optimum imaging in its zone.

[0050] As can also be seen in Figure 5, the inclination of the transducers permits insonification of the breast above the portion immersed in water and beyond the drum. This permits interrogation of the chest tissue surrounding the breast, including the lymphatic system, and thereby provides a more comprehensive scan. The inclination of the transducer also brings the angle of incidence between the signal and surface of the breast closer to 90 degrees, to improve signal penetration and reconstruction

[0051] The circumferential scan may proceed either incrementally position by position or, preferably, on a continuous basis. The rate of scan may be modulated by adjusting the rotational speed of the drum 42 and the resolution adjusted by sampling at multiples of marks on the encoder 70. When the encoder 70 detects the zero position, a full rotation has been achieved and the transducer head 56 is displaced vertically along the Z-axis and the next scan (slice) begins.

[0052] The data acquisition continues until the full vertical scan is complete. The data acquired during scanning from each transducer represents a series of conical slices, which are reconstructed as described above to obtain a three-dimensional ultrasound image of the breast is thus obtained.

[0053] The image quality is enhanced by utilising distal portions of each of the ultrasound signals and by pre-amplifying the received signals on the electronic circuitry **80** carried by the drum and placed in immediate proximity to transducers. This amplification of signal reduces the effect of noise inherent in transmission across the slip ring to result in an increased signal to noise ratio and preserve.

[0054] The scanning system is relatively simple in construction and may be used without specialised installation, supervision and safety measures. The patient support facilitates repeatable image scans. Thus, although a single image may be obtained, the scanner assembly may also be used to obtain images on a periodic basis under comparable imaging conditions. The periodic images can then be compared and changes in detected structure noted. The computer **26** may be remote from the scanning apparatus so that data acquisition may be performed over a telephone connection or similar communication line. If preferred, a communication module may be incorporated into the base allowing the scanner to function as a client in a LAN or other network. In this manner the comparison of images may be performed remotely and the image parameters adjusted remotely to enhance data acquisition. The provision of the network capability also permits multiple scanners to be controlled from a single operator workstation and for data to be acquired and processed centrally.

[0055] The system is designed for non-real time analysis, remote analysis and time series analysis. The support system permits the patient to be scanned in a non-deformed "configuration", where the breast is placed in such a way as to allow for a reasonable ability to repeat the breast position from scan to scan over time. This allows for the scans to be mapped to each other and enables the diagnostician to compare scans and determine whether any changes are occurring in the tissue. The apparatus facilitates the acquisition of such scans in a home or clinic environment with remote monitoring and diagnosis. If further investigation is warranted it may be performed on the same apparatus under different operating parameters, e.g. resolution, or as an alternative form of scan at a specialised facility.

[0056] Although, the system has been described with a breast-imaging scanner, it will be appreciated that it may be adapted for other soft tissue imaging with appropriate modification to the drum and pertinent support.